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After the site has been cleared and grubbed, the lower areas on the western side of the road alignment, between the existing paved roadway and the slopes rising up to the west, should be overexcavated to a depth of 3 feet below the finish road grade, to remove the uncompacted fill in this area. The overexcavation of uncompacted fill will likely be required throughout the new traffic lane area from about Road Sta. 10+00 to Sta. 35+00. The excavated materials may be stockpiled for re—use as fill provided all over—sized material, organics, rubbish, and other deleterious materials are removed in accordance with the Grading recommendations.

2. Site Grading — Once the site has been prepared, grading operations may begin to generate the planned finished grades.

The majority of the excavations required for the retaining wall construction can probably be accomplished with conventional earthmoving equipment. The occasional use of rock excavating equipment, such as hoerams or large, ripper—equipped dozers, should be anticipated to facilitate the removal of massive tuff near the intersection of Salt Lake Boulevard, and random seams of cemented cinders and moderately weathered tuff in the remaining areas.

The excavated on—site soils may be used as fill or backfill provided they are placed and compacted in accordance with these recommendations. The excavated tuff may also be used as fill or backfill provided it is crushed sufficiently to conform to the gradation requirements indicated below for imported fill.

The exposed subgrade in areas to receive fill or structural units, including the overexcavated area resulting from the removal of the uncompacted fill, should be scarified, moisture—conditioned to within 3 percent of the optimum moisture content, and uniformly compacted to at least 90 percent of the soil's maximum dry density as by Laboratory Compaction Test AASHTO T—180, for a minimum depth of 6 inches prior to any fill placement or future construction. Where the exposed subgrade is within 3 feet of the planned finish pavement level, it should be compacted to at least 95 percent relative compaction prior to any fill placement.

Should imported fill be required, it should conform to Section 703.17 of the Standard Specifications and should have a California Bearing Ratio (CBR) greater than 25 when tested in accordance with AASHTO T-193.

Fill and backfill should be placed in uniform lifts of no more than 8 inches in loose thickness, moisture—conditioned to within 3 percent of the optimum moisture content, and uniformly compacted to at least 95 percent relative compaction as determined by the above—referenced test.

Temporary excavations within the cinders which will be required for the retaining wall construction should be sloped back no steeper than 1.5H: 1.0V for heights

of up to 25 feet, or else shored and braced by the contractor. Permanent cut slopes within the massive tuff exposed at the southwestern corner of the intersection of Puuloa Road and Salt Lake Boulevard, may be sloped as steep as 0.5H:1.0V for heights of up to 20 feet. Slopes exceeding these heights are not anticipated at this time and should be individually evaluated, should they occur.

3. Retaining Wall — We believe that the proposed retaining wall can be adequately supported on a continuous strip footing bearing upon properly compacted fill, the medium dense to dense cinders, or the weathered tuff where it may be designed for an allowable bearing capacity of 4,500 p.s.f. This value may be increased by one—third for short—term seismic and wind loads.

The retaining wall footings should have a minimum base width of 5 feet and should be embedded at least 2.5 feet below the lowest adjacent compacted subgrade on level ground.

A friction factor of 0.55 may be used at the contact surface between the bottom of the foundations and the on-site soils to resist sliding.

Keyways cut into the on-site cinders, weathered tuff, or fill placed and compacted in accordance with the grading recommendations may be designed for a passive resistance of 375 pounds per cubic foot (p.c.f.) equivalent fluid pressure. Passive resistance should be disregarded in the top 12 inches of embedment.

The bottom of the footing excavations should be recompacted to at least 95 percent relative compaction as determined by Laboratory Compaction test AASHTO T-180, prior to the placement of concrete and reinforcing steel. Any soft spots encountered in the foundation excavations should be removed and cleaned out to hard natural ground or compacted fill and the resulting depression backfilled in accordance with the Grading recommendations.

Steel reinforcement of the foundations should be provided as recommended by the project structural engineer.

The retaining wall backfill should consist of a well-graded granular fill similar to the on-site cinders. Should imported fill be used as backfill behind the retaining walls, it should conform to the requirements for Aggregate Subbase in Section 703.17 of the Standard Specifications.

The backfill behind the wall should be placed and compacted in accordance with the Grading recommendations. The backfill should be compacted to at least 90 percent but should not exceed 95 percent relative compaction to minimize the lateral earth pressures against the wall.

The earth pressures exerted against the wall will depend on the type and slope of the backfill behind the wall. For wall backfill consisting of the on—site cinders or imported fill conforming to the above recommendation, the estimated active earth pressures are summarized in the following table for various slope conditions.

	Estimated Active	Earth Pressure
Backfill Slope	Horizontal	Vertical
	(p.c.f.)	(p.c.f.)
Level	35	0
3.0H: 1.0V	45	<i>22</i>
2.0H: 1.0V	<i>55</i>	<i>27</i>

The above earth pressures are given in terms of equivalent fluid pressures and do not include surcharge, foundation, or hydrostatic pressures which must be added, where appropriate.

Adequate drainage, in the form of weepholes or transverse drains, should be provided behind the walls to minimize the buildup of hydrostatic pressures.

- A. Transverse drains should consist of perforated pipe surrounded by 6 inches of filter gravel, or AASHTO M43 No. 57 Gravel wrapped in non-woven filter fabric.
- B. Should weepholes be used, a continuous strip of filter gravel, or AASHTO M43 No. 57 Gravel wrapped in filter fabric, measuring at least 12 inches thick by 12 inches in height, should be placed behind the weepholes.
- C. Filter Gravel should conform to Section 703.18 of the Standard Specifications. Non-woven filter fabric should conform to Section 716.03 of the Standard Specifications.

Estimated total_settlements_of_0.8 inch_and estimated differential settlements exceeding 0.3 inch per 20 feet of wall length are not anticipated for foundations designed and constructed in accordance withthese recommendations. The wall and its foundations should be designed to tolerate these estimated settlements.

4. Utilities — Utilities should be installed in accordance with Sections 206, 603, and 604 of the Standard Specifications, and the appropriate section pertaining to each particular utility. Utility backfills should be placed and compacted utilizing the appropriate mechanical compactors above and around the pipes. Jetting and ponding of the backfill should not be allowed.

Utility and similar site excavations should be sloped back, or shored and braced, by the contractor in accordance with DOSH or other applicable governmental regulations. The design of temporary excavations and shoring systems shall be the responsibility of the contractor.

Groundwater was encountered at depths corresponding to about Elev. 2 and Elev. 3 in Borings 6 through 9 of this investigation. Dewatering will be required for utility trenches extending below this level. The design of the dewatering system shall be the responsibility of the contractor.

FED. ROAD DIST. NO.	STATE	FED. AID PROJ. NO.	FISCAL YEAR	SHEET NO.	TOTAL SHEETS
HAWAII	HAW.	STP-7310(1)	2003	7	193

Moderately weathered tuff and cemented cinders will likely be encountered within portions of the deeper utility trench excavations. The occasional use of rock excavating equipment should be anticipated to facilitate the removal of the tuff and cemented cinders.

Utilities may be founded in the properly compacted fill, the medium dense to dense cinders, or the tuff. Where soft spots are encountered at the bottom of utility excavations, they should be removed down to compacted fill or the dense cinders or tuff and the resulting depression replaced with fill compacted in accordance with the grading recommendations. Should boulders or intact tuff be encountered at the pipe invert level, they should be removed in accordance with the Standard Specifications to allow placement of the required Bed Course Material. The Bed Course Material should conform to Section 703.16 of the Standard Specifications.

5. Miscellaneous — Positive drainage provisions should be provided to channel surface waters away from the retaining walls and pavements and preclude the ponding of water adjacent to or beneath the retaining wall, its foundations, and the road pavements. The on—site soils are highly susceptible to erosion. Erosion protection, such as seeding, hydro—mulching, or erosion mats, should be provided as soon as practical after the completion of the grading to minimize erosion within the graded slopes.



STATE OF HAWAII
DEPARTMENT OF TRANSPORTATION
HIGHWAYS DIVISION

GEOTECHNICAL NOTES

THIS WORK WAS PREPARED
BY ME OR UNDER MY
SUPERVISION
Expiration Date of the License:
04/30/04

PUULOA ROAD IMPROVEMENTS Kamehameha Hwy. to Salt Lake Blvd. Federal Aid Project No. STP-7310(1)

Expiration Date of the License: 04/30/04 Scale: As shown

Date: May 2003

SHEET NO. 7 OF 193 SHEETS

FILE: 1600.01 **BORING: BORING:** FILE: 1600.01 FED. AID FISCAL PROJ. NO. YEAR TOTAL SHEETS SHEET NO. STATE PROJECT: PROJECT: PUULOA ROAD WIDENING PUULOA ROAD WIDENING 2003 193 HAW. STP-7310(1) PROJECT ENGINEER: TO MAPUNAPUNA, OAHU, HAWAII PROJECT ENGINEER: TC MAPUNAPUNA, OAHU, HAWAII SURFACE ELEVATION: 25' ± SURFACE ELEVATION: FIELD ENGINEER: 33' ± FIELD ENGINEER: TSK DEPTH TO WATER: DRAFTED BY: DEPTH TO WATER: DRAFTED BY: NONE ENCOUNTERED MD NONE ENCOUNTERED MD F.G.E. LTD. F.G.E. LTD. DATE COMPLETED: DATE COMPLETED: DATE OF DRAWING: DATE OF DRAWING: 3-5-97 3-6-97 MOIST DRY MOIST DRY BLOWS LAB **BLOWS** LAB CONT **TEST** DEN. DEN. PER CLASSIFICATION CLASSIFICATION PCF **RESULTS RESULTS PCF** FILE: 1600.01 FT. **BORING:** PUULOA ROAD WIDENING PROJECT: PROJECT ENGINEER: TC _OCATION: MAPUNAPUNA, OAHU, HAWAII **GRADATION:** GRADATION: REDDISH BROWN SILTY GRAVEL 38 SURFACE ELEVATION: 33' ± FIELD ENGINEER: 48% GRAVEL 25% GRAVEL (GM) WITH SAND, MEDIUM DENSE, **DEPTH TO WATER:** DRAFTED BY: NONE ENCOUNTERED 59% SAND MD 40% SAND GRAYISH BROWN SILTY SAND (SM) WITH GRAVEL, LOOSE TO MEDIUM F.G.E. LTD. 12% DATE COMPLETED: 3-3-97 DATE OF DRAWING: (FILL) SILT/CLAY SILT/CLAY DENSE, MOIST 34 123 NON-PLASTIC S.E. = 62MOIST DRY LAB **BLOWS** (CINDERS) DARK GRAY SILTY SAND (SM) **GRADATION:** TEST CONT DEN. WITH GRAVEL, MEDIUM DENSE TO DENSE, DRY 7% GRAVEL CLASSIFICATION PCF **RESULTS** FT. PH=8.5 51 79 BROWN CLAYEY SILT (ML-CL) WITH SAND, <u>HARD</u>, MOIST 80% SAND (CINDERS) (WEATHERED CINDERS) SILT/CLAY BROWN SILTY GRAVEL (GM) WITH SAND, LOOSE, DAMP 96%REC NX CORE PH=8.0 52%RQD NON-PLASTIC 17 GRAYISH BROWN MODERATELY (CINDERS) WEATHERED GRAYISH BROWN HIGHLY TUFF (WM), HARD, OCCASIONALLY WEATHERED TUFF (WH), BROKEN 30/6" DIRECT 109 BOH @ 13.5' SHEAR: $0 = 36\emptyset$ 8%REC 5%RQD BOH @ 15.0° C=200 PSF GRAYISH BROWN SILTY SAND (SM) WITH GRAVEL AND OCCASIONAL 0.1% SWELL COBBLES, DENSE, DRY TME: D B, FIED: **BORING:** FILE: 1600.01 S.E. = 63**LEGEND** PROJECT: PUULOA ROAD WIDENING GRADES TO MOIST LOCATION: MAPUNAPUNA, OAHU, HAWAII PROJECT ENGINEER: TC MAJOR SOIL TYPES MAJOR ROCK TYPES SURFACE ELEVATION: 27' ± FIELD ENGINEER: DEPTH TO WATER: DRAFTED BY: NONE ENCOUNTERED F.G.E. LTD. **GRAVEL** BASALT DATE COMPLETED: 3-6-97 DATE OF DRAWING: 50/6" 27 83 DRY BLOWS MOIST LAB (CINDERS) DEN. PCF **TEST** PER FT. TUFF SAND CLASSIFICATION RESULTS GRAYISH BROWN CLAYEY SILT (ML—CL), <u>HARD</u>, MOIST BROWN CLAYEY SILT (MH) WITH DECOMPOSED SILT GRAVEL, STIFF, MOIST DIRECT SHEAR: 55 73 49 (COMPLETELY WEATHERED TUFF) ROCK 72 S.E.=14 39 (FILL) **GRADATION:** BOH @ 25.0' 0 = 45059% GRAVEL BROWN SILTY GRAVEL (GM) WITH SAND, LOOSE, MOIST C=200 PSF CORAL 30% SAND 2.0% SWELL (FILL) SILT/CLAY **SECONDARY** 24 97 CLASSIFICATION PEAT/ORGANICS ___30 SHEAR: 0 = 320**GRAVELLY** C=850 PSF SAMPLING SYMBOLS 0.8% SWELL GRAYISH BROWN CLAYEY SILT (ML-CL) WITH SAND AND GRAVEL, VERY STIFF TO HARD, DAMP LL=49,PI=22 3" O.D. UNDISTURBED PH=8.1 STATE OF HAWAII SAMPLE DEPARTMENT OF TRANSPORTATION SANDY 3" O.D. DISTURBED LICENSED PROFESSIONAL ENGINEER NX-CORE HIGHWAYS DIVISION SAMPLE Survey Plo Drawn by Traced by Designed b Quantities 2" O.D. STANDARD BORING LOGS No.8418-C 33 26 93 (WEATHERED CINDERS) PENETRATION SAMPLE SILTY BOH @ 15.0' <u>NO</u> RECOVERY PUULOA ROAD IMPROVEMENTS WATER V Kamehameha Hwy. to Salt Lake Blvd. <u>SHELBY</u> <u>TUBE</u> THIS WORK WAS PREPARED
BY ME OR UNDER MY
SUPERVISION CLAYEY Federal Aid Project No. STP-7310(1) BAG SAMPLE Expiration Date of the License: Scale: As shown Date: May 2003 SHEET NO. 8 OF 193 SHEETS

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LL=54, PI=20 Direct Shear:		474 249	53 1.7	1		Brown Clayey SILT (MH) with Gravel, hard, damp (FILL)	Gradation: 27% Gravel 26% Sand 47% Silt/Clay Gradation: 43% Gravel	14	490 650	41 25	2	<u>-</u>	with Sand, medium <u>dense</u> , <u>moist</u> (FILL) Tan Silty Coral GRAVEL (GM) with sand, medium <u>dense</u> ,	F.G.E. Ltd. LAB TEST	Date C MOIST CONT.		ed: BLOWS PER	3-3-9	incounter 7 D E P	ed	Date	fted by: e of Drav	wing:
0=35ø C=150 psf 2.7% Swell LL=37,PI=13 Consol.		314	10 8 42		· · · · · · · · · ·	Brown Clayey SILT (ML—CL) with Sand and Gravel, very stiff, damp (FILL) Brown Clayey SILT (ML—CL) with some Sand and Grave very stiff, moist (ALLUVIUM) Grayish Brown Clayey SILT (ML—CL), hard, saturated (COMPLETELY WEATHERED TUFF BOH @ 15.0'	41% Sand 16% Silt/Clay pH=9.2	37		R R 98%REC 31%RQD	4		with Gravel, very <u>dense,</u> <u>saturated</u> (CINDERS)	RESULTS			57/9" R 93%REC 0%RQD 83%REC 25%RQD	NX CORE	- 1 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5 - 5	W G N T	Prown Silty with Sand Frayish Bro Moderately UFF (WM),	/ GRAVE	EL (GM) (CINDE
F.G.E. Ltd.	Depth	t: F	er:		Hawai	, , ,	F.G.E. Ltd.	Boring: Project Location Surfact Depth Date (t: I on: I e Eleva to Wat	er:		, Hawaii	File: 1600.01 Project Engineer: TC Field Engineer: TSK Drafted by: MD Date of Drawing:				48%REC 0%RQD 2%REC 0%RQD			(Trayish Bro SM) with ccasional	Gravel d	and
LAB TEST RESULTS	MOIST CONT. %	DRY DEN. PCF	BLOWS PER FT.	SAMPLIE	DEPTH	CLASSIFICATION	LAB TEST RESULTS	MOIST CONT. %	DRY DEN. PCF	BLOWS PER FT.	SAMPLE	DEPTH	CLASSIFICATION				60%REC 0%RQD	NX CORE	- - - - - - - - - - - - - - - - - - -	S	rayish Bro ILT (ML-C ravel, <u>har</u>	CL) with d, mois	
S.E.=16 LL=46,PI=7 Gradation: 30% Gravel	32	169	24 28 25	1 2 3	5	Light Brown Clayey SILT (ML-CL) with Gravel, very stiff, moist (FI Brown Silty SAND (SM) with Gravel, medium dense, moist	non-plastic 0.0% Swell S.E.=33		121 2050	38 23 65	1 2 3	5	Dark Brown Clayey SILT (ML−CL) with Gravel, very stiff, damp (FILL) Dark Brown Silty GRAVEL (GM) with Sand and Cobbles, medium dense to dense, damp (FILL)								•	BOH @	
47% Sand 23% Silt/Clay pH=8.3			15 82	4	- 10 - 15 - 15	Grayish Brown Clayey SILT (ML-CL) with Sand, very stiff, moist Gray Silty SAND (SM) with Gravel, dense,	JM)			3	5	70	Dark Gray Silty SAND AND GRAVEL (GM—GW), very loose, saturated (LAGOON) BOH @ 15.0'				PROFIEN NO.8	MURAN PREPARED R UNDER MY RVISION	F Kame	E PUULOA ehamel	-	LOGS MPROVEN o Salt	
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